

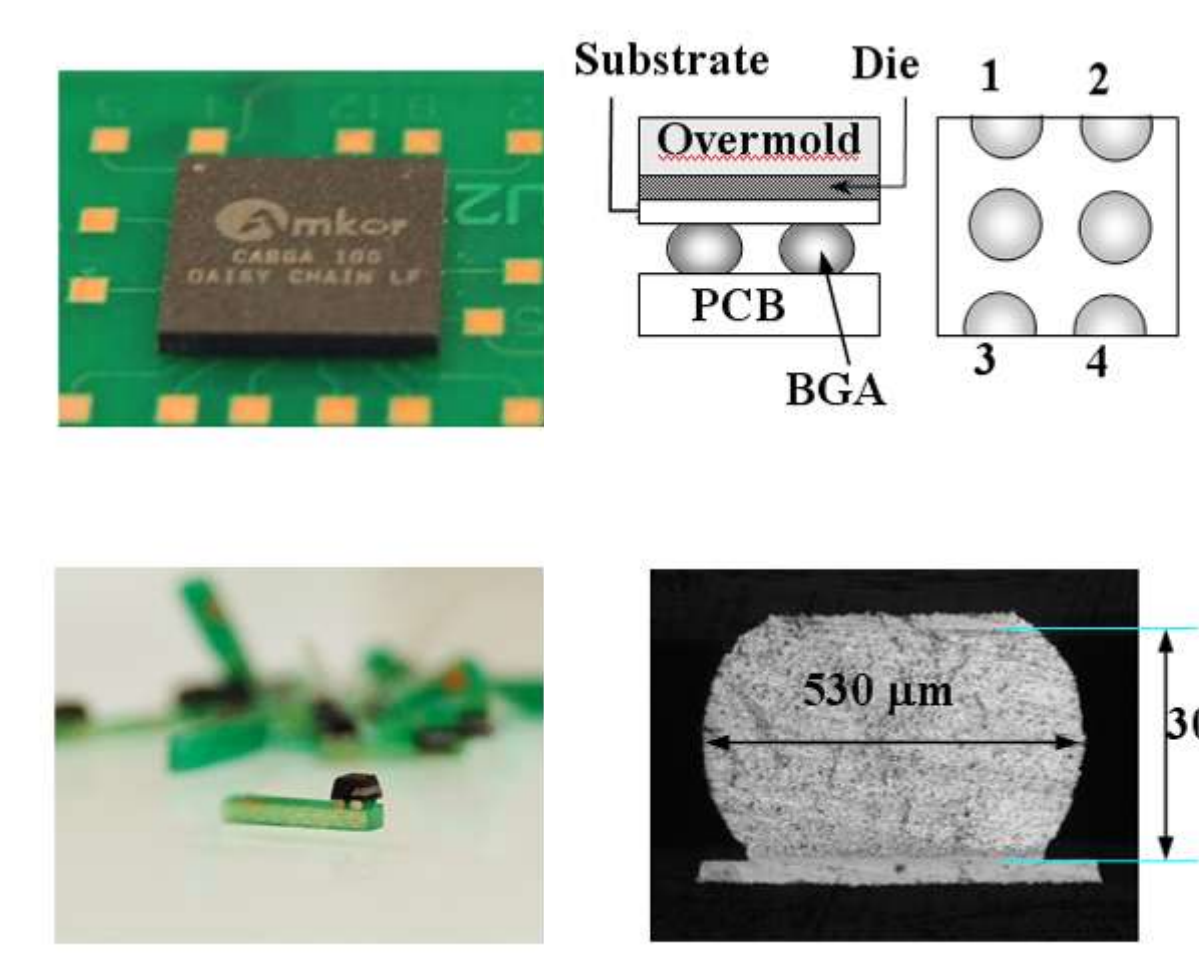
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## INTRODUCTION

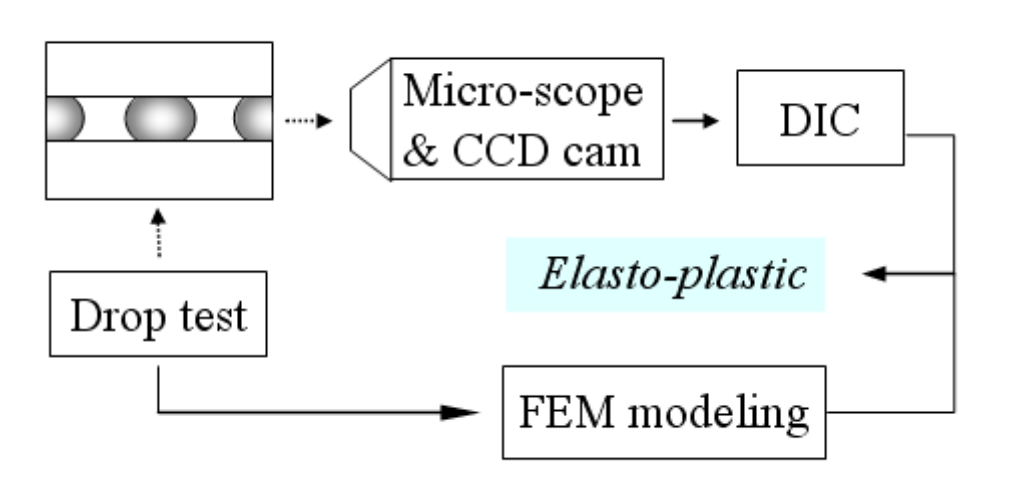
1. Material properties of SAC are needed to support modeling
  - Elastic, time-independent, time-dependent plastic (creep)
2. Why actual solder joints?
  - Bulk solder and solder joints have different microstructures
3. State-of-the art
  - There are many published data for bulk solder
  - However, data for actual solder joints are not available yet
4. Elastic and time-independent plastic properties of SAC105, SAC305, and SAC405 were measured in this work
5. Methodology
  - Combining compressive, drop test, DIC and FEM modeling

## TEST VEHICLE



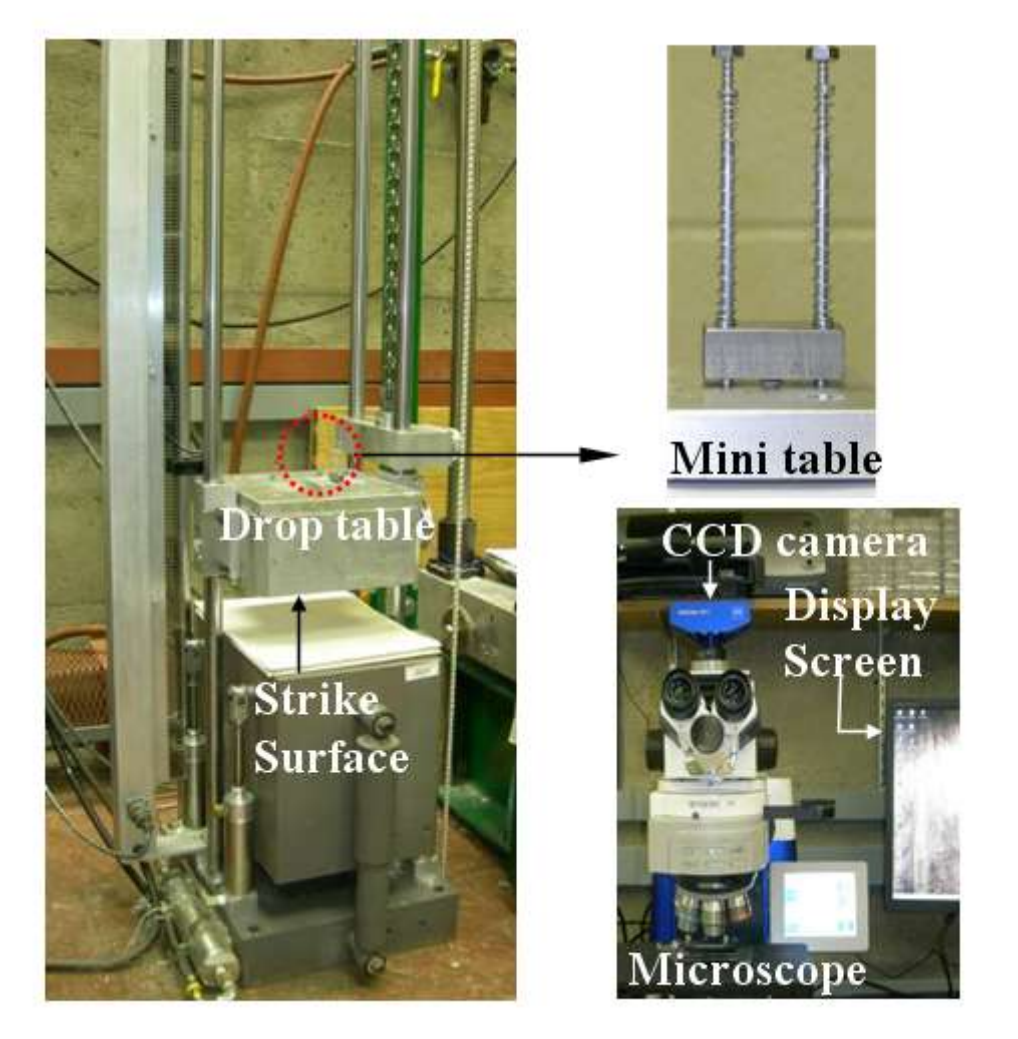
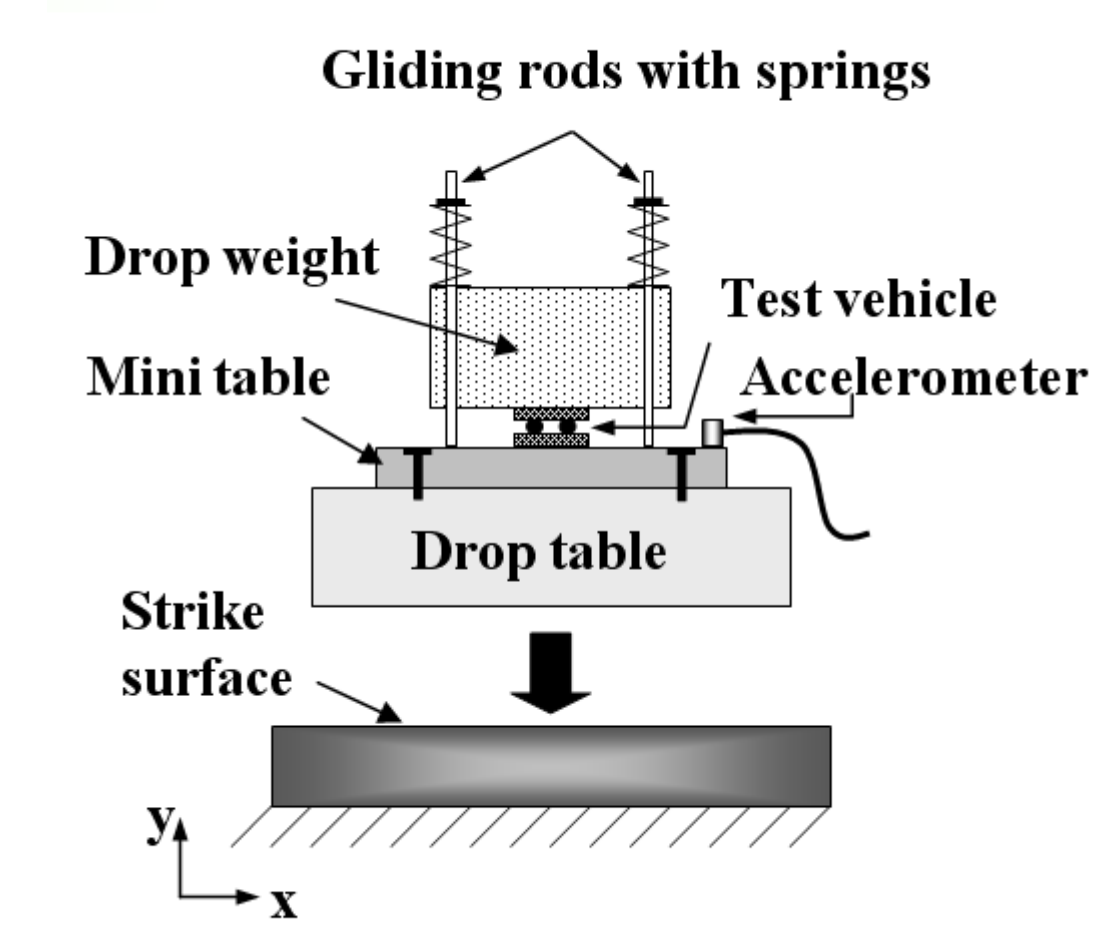
- The test vehicle: CABGA
- Packages were cross-sectioned & polished using 320-1200 grit silicon carbide papers
- Cross-sectioned surfaces exhibit random speckle pattern for DIC → No further treatment is needed

## EXPERIMENTS



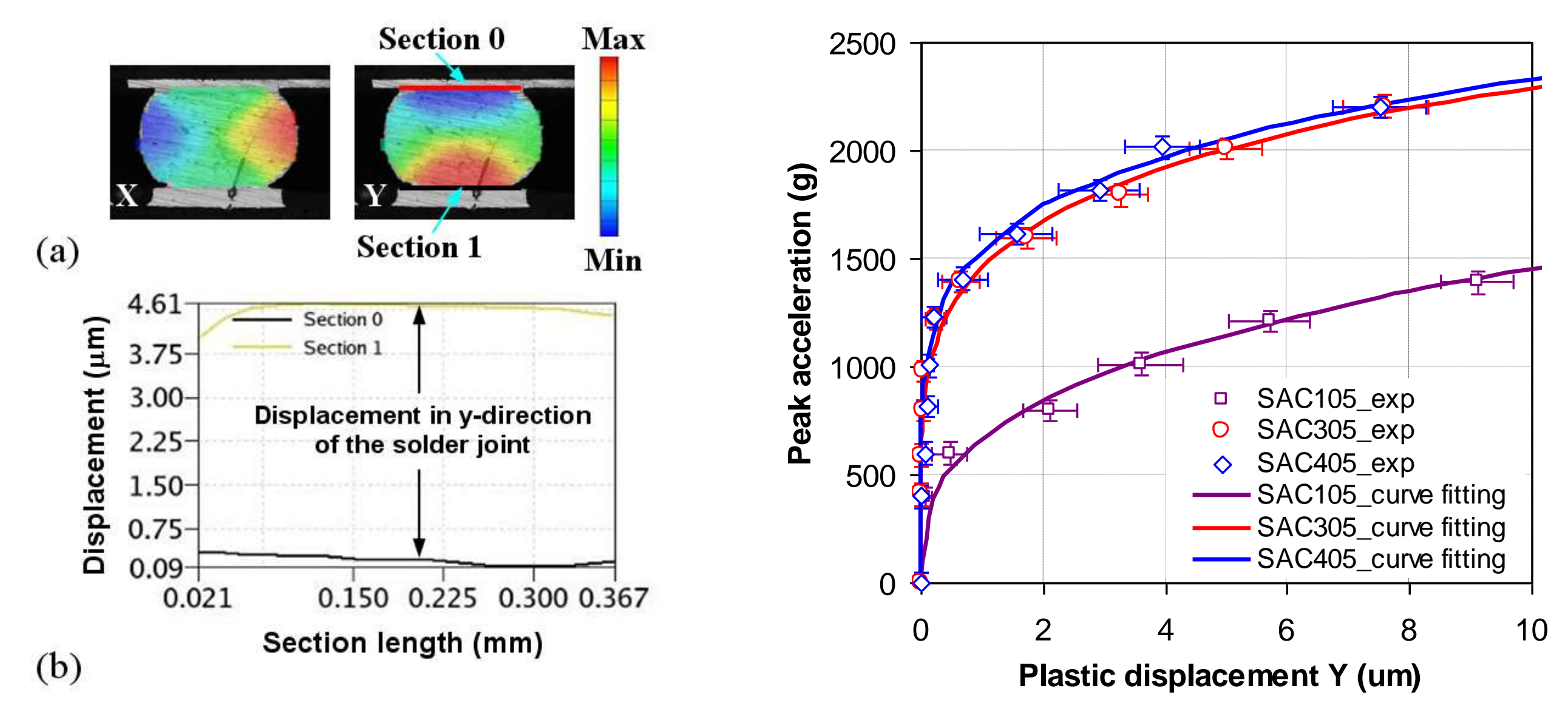
- Drop weight technique was used to create compressive force on the BGA
- Images of solder joints were taken before and after each drop using microscope

- Plastic displacement & strain in the BGA were evaluated using DIC
- A mini-table was specially designed for the drop tests
- An accelerometer was used to monitor the transient acceleration
- Drop tests with peak acceleration 400G–3000G were performed



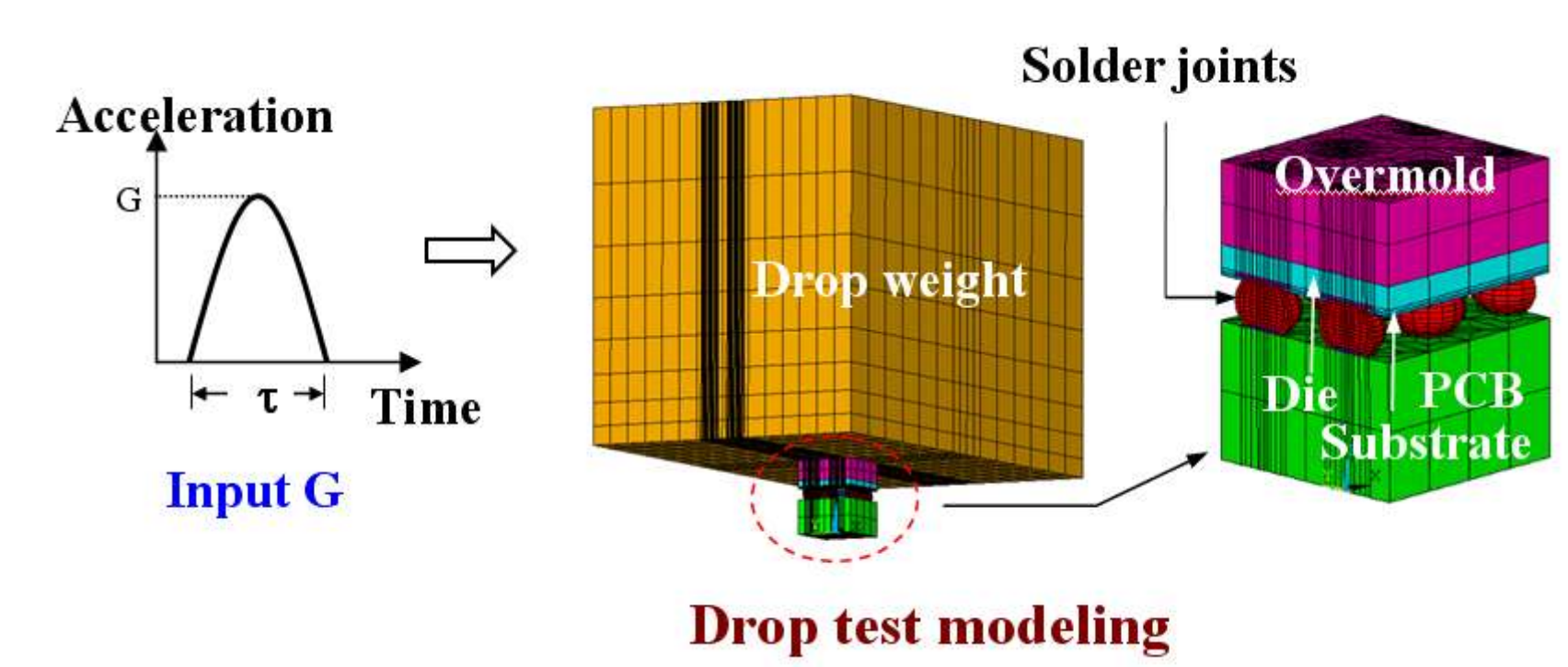
## EXPERIMENTAL RESULTS

- Contour plot depicts well behavior of BGA under compression
- Displacement Y: Difference between values of section 0 and 1
- Displacement of a sample is the mean value of the solder balls
- No separation of elastic plastic displacements is needed



## FEM MODELING

- Analysis: Transient
- Method: "G-Input"
- Elasto-plastic model: Multi-linear kinematic hardening (TB,KINH) for the solder joints



## ITERATION PROCESS

- Ramberg-Osgood Equation

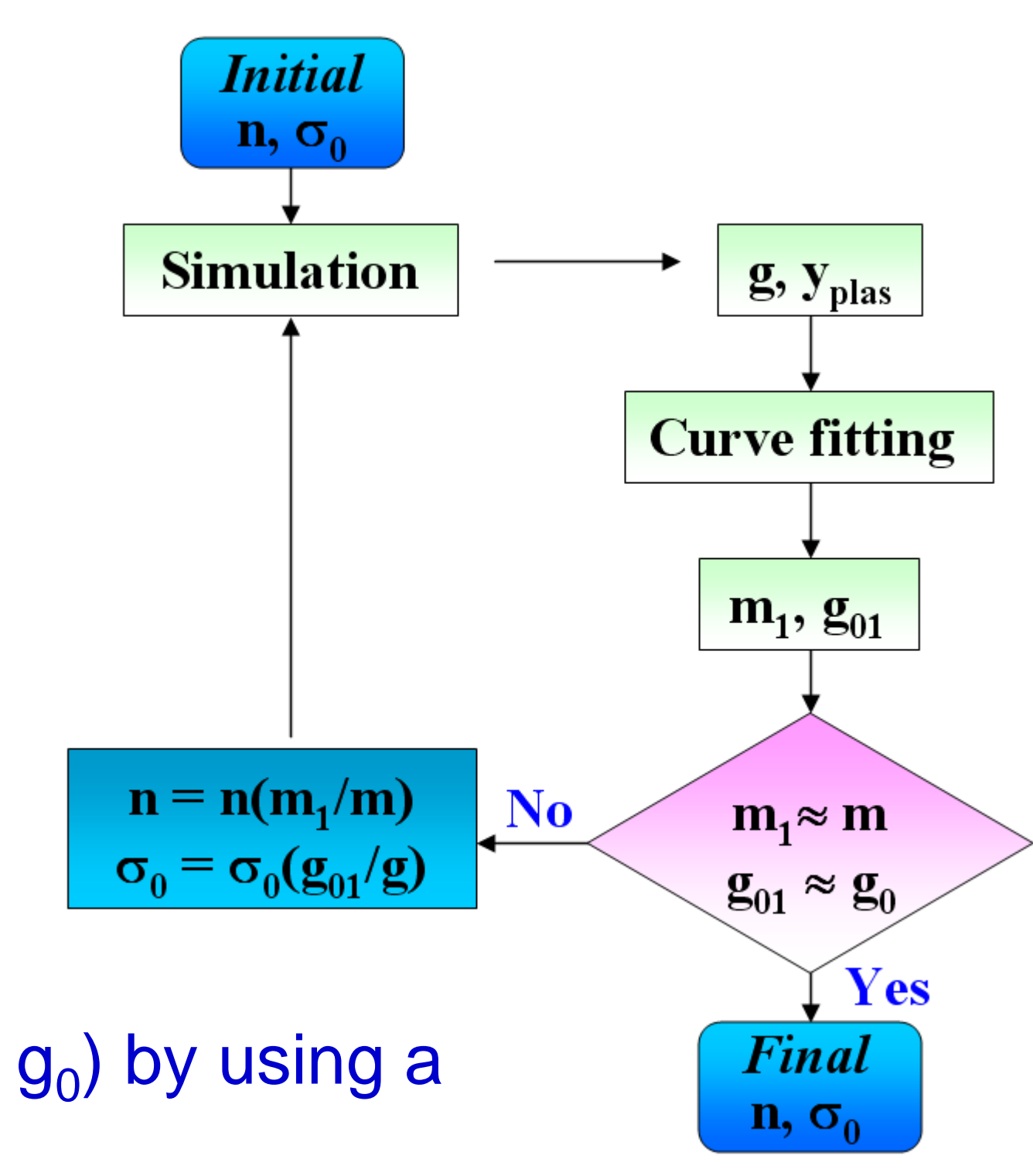
$$\varepsilon = \frac{\sigma}{E} + \left(\frac{\sigma}{\sigma_0}\right)^n$$

- Curve fitting ( $G, Y_{plas}$ )

$$y_{plas} = \alpha \left(\frac{g}{g_0}\right)^m$$

- ( $m, g_0$ ) were obtained by fitting the experimental data

- ( $n, \sigma_0$ ) were extracted from ( $m, g_0$ ) by using a developed iteration process



## RESULTS & DISCUSSIONS

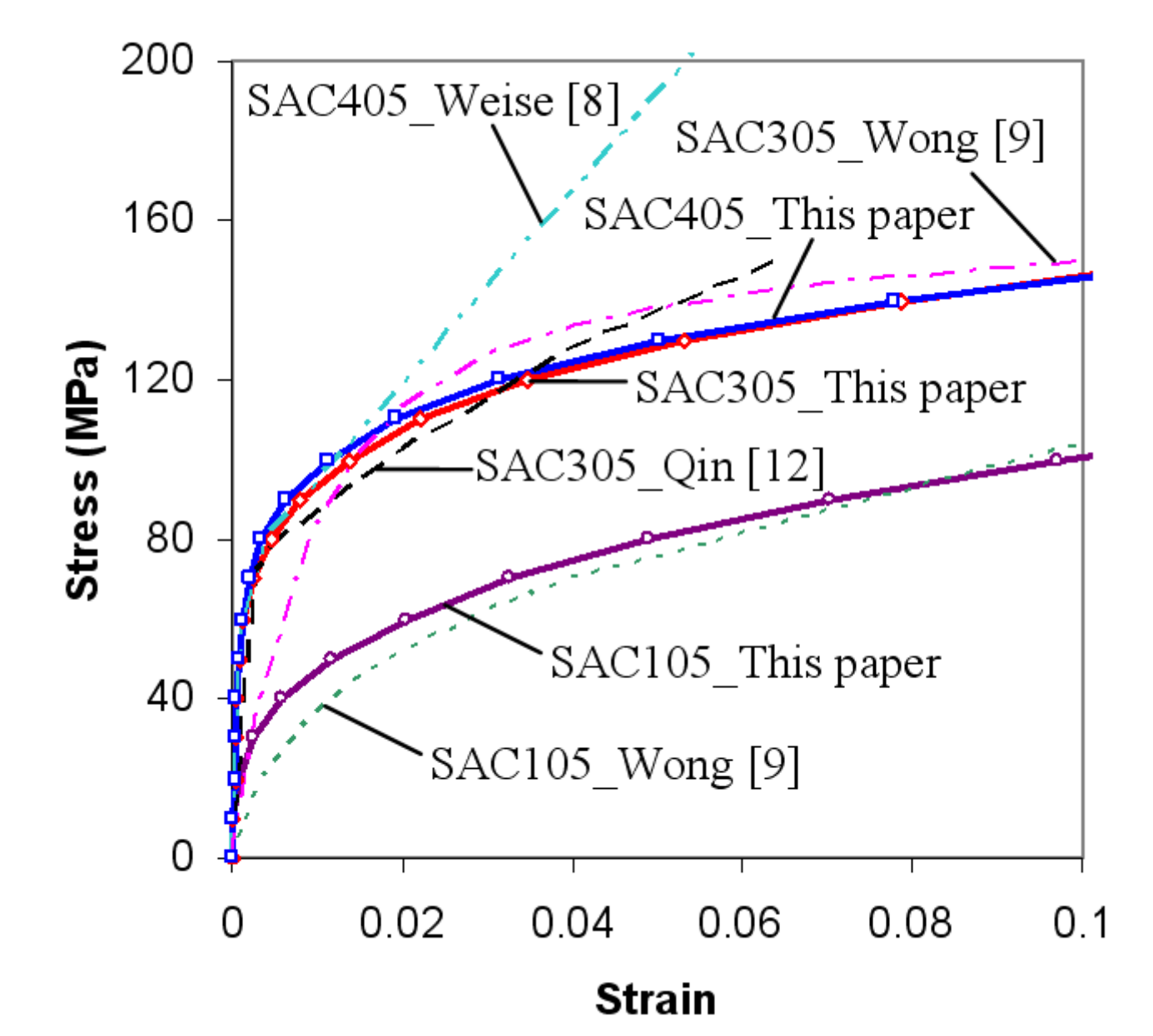
### Constitutive Equations

SAC105  $\varepsilon = \frac{\sigma}{97} + \left(\frac{\sigma}{213}\right)^{3.1}$

SAC305  $\varepsilon = \frac{\sigma}{90} + \left(\frac{\sigma}{232}\right)^{5.4}$

SAC405  $\varepsilon = \frac{\sigma}{86} + \left(\frac{\sigma}{215}\right)^6$

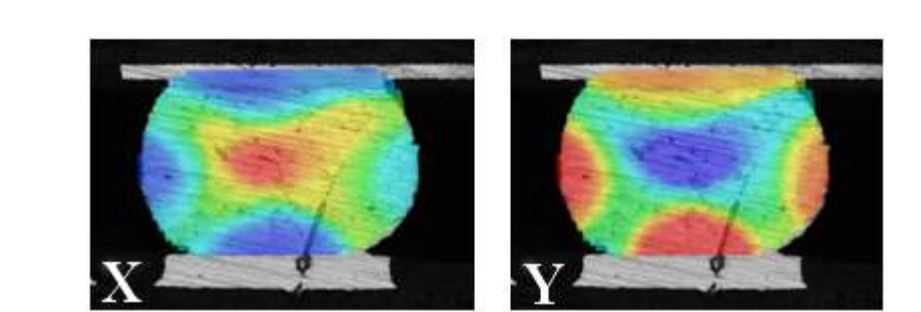
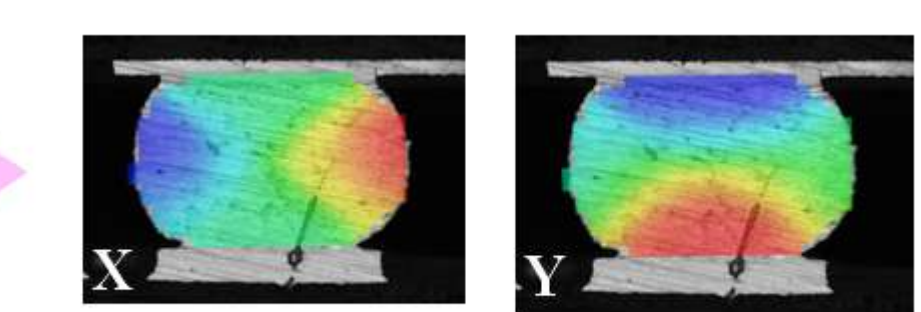
### Stress-strain curves



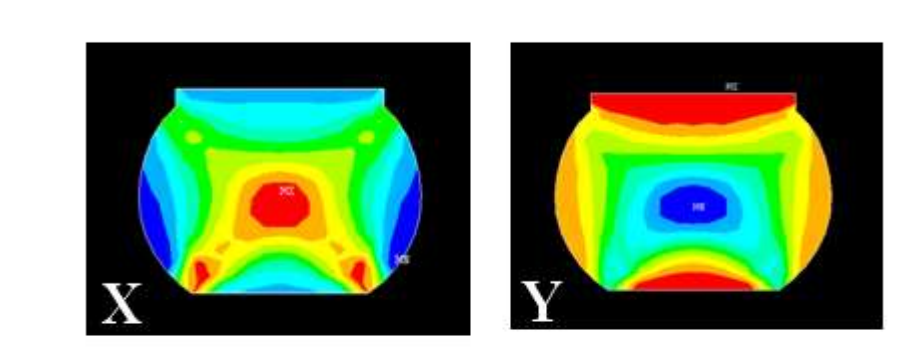
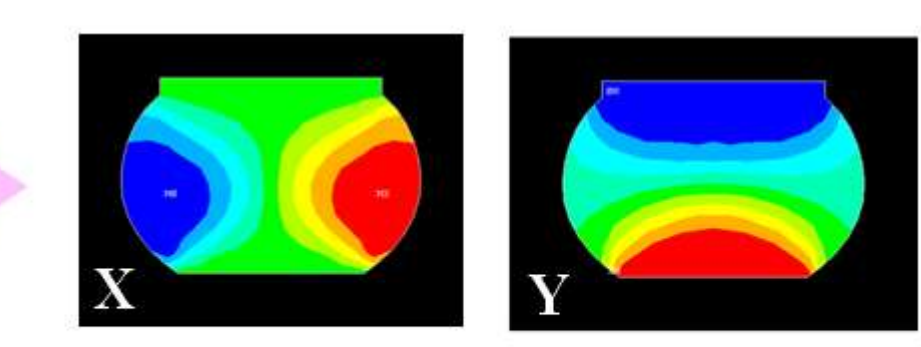
### Plastic displacement

### Plastic strain

Experimental



Numerical



- Constitutive equations for SAC105, SAC305, and SAC405 solder joints were successfully developed
- The results in this work are in good agreement with literature
- Contour plots from DIC and drop modeling match very well

## CONCLUSIONS

- A novel methodology was developed for the characterization of elasto-plastic behavior of SAC solder alloys
- The Ramberg-Osgood model is able to describe the elasto-plastic behavior of the solder alloys
- The coefficients of the model were successfully extracted with high accuracy
- The model was recommended to be used for drop test modeling of electronic packaging

## ACKNOWLEDGEMENT

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